

# WAVE RESISTANCE IN DEEP WATER DUE TO THE ACCELERATED MOTION OF A PRESSURE SYSTEM

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1. We have seen in a previous paper (Bhattacharya, 1956) which will henceforth be called paper I, that when a pressure system  $H(\bar{\omega})$ , symmetrical about the origin starts with an initial velocity  $c$ , and moves over the surface of deep water with uniform acceleration  $f$ , the surface elevation of the waves that are generated is given by

$$\pi g \rho y = \int_0^\infty k V \psi(k) \exp(ik\bar{\omega}) dk \int_0^t \sin kV\tau \exp[-\mu\tau + ik\{c\tau + \frac{1}{2}f\tau(2t-\tau)\}] \times d\tau \quad \dots (1.1)$$

where

$$\begin{aligned} \psi(k) &= \int_{-\infty}^\infty H(\bar{\omega}) \exp(-ik\bar{\omega}) d\bar{\omega} \\ &= 2 \int_0^\infty H(\bar{\omega}) \cos k\bar{\omega} d\bar{\omega}. \quad \dots \quad \dots \quad \dots (1.2) \end{aligned}$$

We define, after Havelock (1917), the wave resistance as the total horizontal component of the pressure over the wetted area of the ship, which by our hypothesis is represented by the moving pressure system.

In Fig. 1,  $\bar{\omega}$ -axis represents the undisturbed surface,  $y$  the vertical axis, and the curve a depression of the free surface.

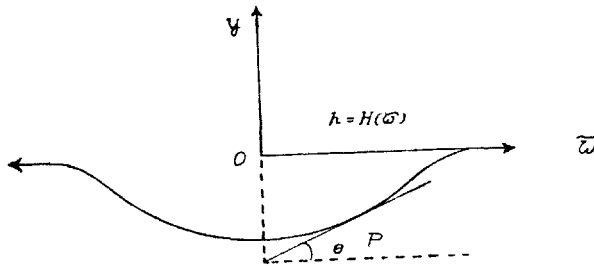


FIG. 1

The horizontal component of the pressure at a point of the free surface is

$$-p \sin \theta = -p \tan \theta = -H(\bar{\omega}) \frac{\partial y}{\partial \bar{\omega}},$$

for  $\theta$  is small.

We define the wave resistance by

$$R = \int_{-\infty}^{\infty} H(\bar{\omega}) \frac{\partial y}{\partial \bar{\omega}} d\bar{\omega}. \quad \dots \dots \dots (1.3)$$

In this integral  $y$  will be replaced by its three parts,

$$y = y_1 + y_2 + y_3 \quad \dots \dots \dots (1.4)$$

worked out in paper I referred to above and the parts of the resistance arising out of  $y_1$ ,  $y_2$  and  $y_3$  will be called  $R_1$ ,  $R_2$  and  $R_3$  respectively, so that the total resistance will be given by

$$R = R_1 + R_2 + R_3. \quad \dots \dots \dots (1.5)$$

### 2. Calculation of $R_1$

This is simple and straightforward. It has been shown in paper I that

$$\pi g \rho y_1 = f(\bar{\omega}), \text{ for } \bar{\omega} > 0$$

and

$$= 2\pi k_0 \psi(k_0) \sin k_0 \bar{\omega} + f(-\bar{\omega}), \text{ for } \bar{\omega} < 0,$$

with

$$k_0 = g/v^2.$$

Substituting  $y_1$  for  $y$  in (1.3) and noticing that the symmetrical part  $f(\bar{\omega})$  of  $y_1$  contributes nothing to  $R_1$ , we have

$$\begin{aligned} \pi g \rho R_1 &= \int_{-\infty}^0 H(\bar{\omega}) \cdot 2\pi k_0^2 \psi(k_0) \cos k_0 \bar{\omega} d\bar{\omega} \\ &= 2\pi k_0^2 \psi(k_0) \int_0^{\infty} H(\bar{\omega}) \cos k_0 \bar{\omega} d\bar{\omega} \\ &= \pi k_0^2 \{\psi(k_0)\}^2, \end{aligned}$$

by (1.2) and the symmetry of  $H(\bar{\omega})$  about the origin.

Then

$$\begin{aligned} R_1 &= \frac{k_0^2}{g\rho} \left\{ \psi(k_0) \right\}^2 \\ &= \frac{g}{\rho v^4} \left\{ \psi(k_0) \right\}^2. \quad \dots \dots \dots (2.1) \end{aligned}$$

### 3. Calculation of $R_2$

In obtaining  $R_2$  we might proceed as in the case of  $R_1$ . But the expression for  $y_2$  is much too complicated for further differentiation and integration. We therefore fall back upon the earlier integral given in (1.1). We note that the time integral involved in (1.1) is

$$\int_0^t \sin kV\tau \cdot \exp \left[ -\mu\tau + ik \left\{ c\tau + \frac{1}{2}f\tau(2t-\tau) \right\} \right] d\tau. \quad \dots \dots (3.1)$$

It has been shown in paper I that the part of the integral (3.1) which yields  $y_2$  is given by

$$-\frac{1}{2k} \exp[ik(vt - \frac{1}{2}ft^2)] \left\{ \frac{\exp(ikVt)}{v+V} - \frac{\exp(-ikVt)}{v-V} \right\} \dots \quad (3.2)$$

when  $\mu \rightarrow 0$ .

This will be responsible for  $R_2$ . To calculate this, however, we go back to our original equation (1.1), and the definition of total resistance  $R$  in (1.3). These two equations together give

$$\begin{aligned} \pi g \rho R = -i \int_0^\infty k^2 V \{ \psi(k) \}^2 dk \int_0^t \sin kV\tau \times \\ \exp \left[ -\mu\tau + ik \left\{ c\tau + \frac{1}{2}f\tau(2t-\tau) \right\} \right] d\tau. \dots \quad (3.3) \end{aligned}$$

Now if in this integral we replace the time-integral part of it by (3.2), we obtain

$$\begin{aligned} \pi g \rho R_2 = \frac{i}{2} \int_0^\infty kV \{ \psi(k) \}^2 \exp(ikd) \left\{ \frac{\exp(ikVt)}{v+V} - \frac{\exp(-ikVt)}{v-V} \right\} d\tau \\ = \frac{1}{2} i(A-B) \dots \dots \dots \quad (3.4) \end{aligned}$$

where

$$A = \int_0^\infty \frac{kV \{ \psi(k) \}^2}{v+V} \exp \{ ik(d+Vt) \} dk, \dots \dots \quad (3.5)$$

$$\begin{aligned} d &= vt - \frac{1}{2}ft^2 \\ &= ct + \frac{1}{2}ft^2 \\ &= \text{distance travelled by the moving pressure system in} \\ &\quad \text{time } t, \text{ and} \end{aligned}$$

$$B = \int_0^\infty \frac{kV \{ \psi(k) \}^2}{v-V} \exp \{ ik(d-Vt) \} dk. \dots \dots \quad (3.6)$$

Now after a little reduction we obtain

$$A = 2(k_0)^{\frac{1}{2}} \int_0^\infty \phi(u) e^{if(u)} du, \dots \dots \quad (3.7)$$

where

$$\begin{aligned} \phi(u) &= u^3 \{ \psi(u^2) \}^2 / (u + \sqrt{k_0}), \\ f(u) &= d.u^2 + pu \text{ and } p = g^{\frac{1}{2}}t. \end{aligned}$$

This gives

$$f'(u) = 2du + p,$$

so that

$$\alpha = (\text{a root of } f'(u) = 0) = -p/2d = -Ve.$$

By Kelvin's group approximation method (Lamb, 1932) contribution to the integral (3.7) comes only from  $\alpha$ , and as  $\alpha$  lies outside the range of integration,  $A = 0$ . Hence

$$\pi g \rho R_2 = -\frac{1}{2}iB$$

where after some reduction we obtain

$$B = 2(k_0)^{\frac{1}{2}} \int_0^\infty \phi(u)e^{if(u)} du, \dots \dots \dots (3.8)$$

where

$$\phi(u) = u^3 \{ \psi(u^2) \}^2 / (u - \sqrt{k_0}),$$

and

$$f(u) = du^2 - pu.$$

It may be observed that the principal value of this integral exists and can be evaluated by Kelvin's group approximation method; the contribution comes from  $\alpha = p/2d$ , which is a root of  $f'(u) = 0$ .

Thus we get

$$B = 2\sqrt{k_0} \cdot \frac{\sqrt{\pi}\phi(\alpha)}{\sqrt{|\frac{1}{2}f''(\alpha)|}} \exp \left[ i \left\{ f(\alpha) \pm \frac{\pi}{4} \right\} \right],$$

the upper or the lower sign in the exponential being taken according as  $f''(\alpha)$  is +ve or -ve respectively.

From the above formula, taking the real part only, we have

$$\rho R_2 = - \frac{i^2 \sqrt{g}}{4c\pi^{\frac{1}{2}} d^{\frac{3}{2}}} \left\{ \psi(p^2/4d^2) \right\}^2 \sin \left( \frac{\pi}{4} - \frac{p^2}{4d} \right). \dots \dots (3.9)$$

#### 4. Calculation of $R_3$

To get  $R_3$  we proceed as in the case of calculation of  $R_2$ . The part of the time-integral in (1.1) which gives rise to  $y_3$  and hence to  $R_3$  is given by

$$- \frac{1}{2i} \left( \frac{2\pi}{kf} \right)^{\frac{1}{2}} \exp \left[ i \left\{ \frac{k(v^2 + V^2)}{2f} - \frac{\pi}{4} \right\} \right] \exp(-ikvV/f). \dots (4.1)$$

Again replacing the time-integral part of (3.3) by (4.1) we get

$$\begin{aligned} \pi g \rho R_3 &= \frac{1}{2} \left( \frac{2\pi g}{f} \right)^{\frac{1}{2}} \int_0^\infty k \{ \psi(k) \}^2 \exp \left[ i \left\{ \frac{k(v^2 + V^2)}{2f} - \frac{\pi}{4} \right\} \right] \\ &\quad \times \exp(-ikvV/f) dk. \end{aligned}$$

Putting  $V^2 = g/k$ , the above expression reduces to

$$\begin{aligned} &\frac{1}{2} \left( \frac{2\pi g}{f} \right)^{\frac{1}{2}} e^{i \left( \frac{g}{2f} - \frac{\pi}{4} \right)} \int_0^\infty k \{ \psi(k) \}^2 e^{i \left( \frac{v^2}{2f} k - \frac{vg}{f} k^{\frac{1}{2}} \right)} dk \\ &= \left( \frac{2\pi g}{f} \right)^{\frac{1}{2}} e^{i \left( \frac{g}{2f} - \frac{\pi}{4} \right)} \int_0^\infty u^3 \{ \psi(u^2) \}^2 e^{i (d_1 u^2 - p_1 u)} du \\ &= \left( \frac{2\pi g}{f} \right)^{\frac{1}{2}} e^{i \left( \frac{g}{2f} - \frac{\pi}{4} \right)} \int_0^\infty \phi(u) e^{if(u)} du. \dots \dots \dots (4.2) \end{aligned}$$

where we have put

$$d_1 = v^2/2f, p_1 = vg^{\frac{1}{2}}/f, \phi(u) = u^3 \{ \psi(u^2) \}^2,$$

and

$$f(u) = d_1 u^2 - p_1 u.$$

Evaluating (4.2) again by Kelvin's group approximation method we have

$$\pi g \rho R_3 = \left(\frac{2\pi g}{f}\right)^{\frac{1}{2}} e^{i\left(\frac{g}{2f} - \frac{\pi}{4}\right)} \frac{\sqrt{\pi \phi(\alpha)}}{\sqrt{|\frac{1}{2}f''(\alpha)|}} e^{i\left\{f(\alpha) + \frac{\pi}{4}\right\}}$$

where  $\alpha = p_1/2d_1$  is obtained from  $f'(\alpha) = 0$ .

Further as

$$f''(\alpha) = 2d_1, \quad f(\alpha) = -p_1^2/4d_1,$$

and

$$\phi(\alpha) = p_1^3 \{\psi(p_1^2/4d_1^2)\}^2/8d_1^3$$

we get after some simplification

$$\begin{aligned} \rho R_3 &= \frac{2g}{v^4} \left\{ \psi(p_1^2/4d_1^2) \right\}^2 \exp \left\{ i \left( \frac{g}{2f} - \frac{p_1^2}{4d_1} \right) \right\} \\ &= \frac{2g}{v^4} \left\{ \psi(g/v^2) \right\}^2 = 2k_0^2 \{ \psi(k_0) \}^2 \\ &= 2\rho R_1. \end{aligned}$$

$$\therefore R_3 = 2R_1. \quad \dots \dots \dots (4.3)$$

5. Numerical tables for  $R_1$ ,  $R_2$  and  $R_3$

Let us choose

$$\psi(k) = Av^2 \exp(-\gamma k). \quad \dots \dots \dots (5.1)$$

Then from (2.1)

$$\rho R_1 = A^2g \exp(-2\gamma k_0). \quad \dots \dots \dots (5.2)$$

From (3.9) and (5.1) we have

$$\rho R_2 = -\frac{Ag^{\frac{1}{2}}t^2v^4}{4c\pi^{\frac{1}{2}}d^{\frac{5}{2}}} \exp(-\gamma p^2/2d^2) \sin\left(\frac{\pi}{4} - \frac{p^2}{4d}\right). \quad \dots \dots (5.3)$$

Taking  $A = 1$ ,  $\gamma = 1$ , we have

$$\begin{aligned} \rho R_2 &= -\frac{8(c+ft)^4 \exp(-p^2/2d^2) \sin\left(\frac{\pi}{4} - \frac{p^2}{4d}\right)}{c\pi^{\frac{1}{2}}t^{\frac{1}{2}}(2c+ft)^{\frac{5}{2}}} \\ &= -\rho \underline{R}_2 \sin\left(\frac{\pi}{4} - \frac{p^2}{4d}\right), \quad \dots \dots \dots (5.3a) \end{aligned}$$

where  $\underline{R}_2$  is the amplitude of  $R_2$ , so that

$$\rho \underline{R}_2 = 8(c+ft)^4 \exp(-p^2/4d^2)/c \sqrt{\pi t(2c+ft)^{\frac{5}{2}}}. \quad \dots \dots (5.4)$$

$R_3$  is given in terms of  $R_1$  by (4.3).

In addition to  $A = 1$ , and  $\gamma = 1$ , let us take  $c = 2.5$  ft./sec.,  $f = \frac{1}{4}$  ft./sec.<sup>2</sup>, and tabulate  $R_1$ ,  $\underline{R}_2$  and  $R_3$  as given by (5.2), (5.4) and (4.3) between the times 5 and 60 seconds.

TABLE I  
For  $\rho R_1$ ,  $\rho R_2$ ,  $\rho(R_1+R_3)$

$t$	5	10	15	20	25	30	35	40	45	50	55	60
$\rho R_1$	·34	2·47	6·19	10·26	13·87	16·87	19·30	21·25	22·81	24·08	25·11	25·97
$\rho R_2$	1·38	2·18	2·99	3·83	4·85	5·84	6·85	7·88	8·79	9·98	11·04	12·12
$\rho(R_1+R_3)$	1·02	7·41	18·57	30·78	41·61	50·61	57·90	63·75	68·43	72·24	75·33	77·91

Since  $R_3 = 2R_1$ ,  $R_1+R_3 = 3R_1$ , the entries in the last row have been obtained by multiplying the corresponding entries in the first row by 3. The actual graph of  $\rho R_2$  is an oscillating curve of moderate frequency lying between  $\pm \rho R_2$ . The graph of  $\pm \rho R_2$  is shown by the bounding curves in Fig. 2. From the tables it is clear that  $R_2$  is small in comparison with the other parts.

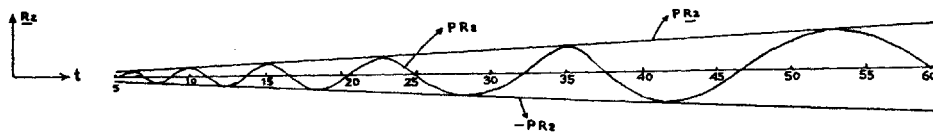


FIG. 2

Both  $R_1$  and  $R_3$  go on increasing with time but  $R_3$  dominates over the other components.  $R_3$ , which is the special contribution of the acceleration, lasts as long as the acceleration lasts. Although it is the special effect of acceleration, it does not depend purely on the acceleration but, like  $R_1$ , is determined by the instantaneous velocity. But for reasons given in paper I (p. 159),  $R_3$  would disappear if the acceleration vanishes while  $R_1$  would persist in that case also.

#### 6. Zeros, humps and hollows of $R_2$

We have from (5.3a) and (5.4)

$$R_2 = \underline{R}_2 \sin \theta$$

where  $\underline{R}_2$  has been graphed before and

$$\theta = \frac{p^2}{4d} - \frac{\pi}{4} = \frac{64t}{20+t} - \frac{\pi}{4},$$

where use has been made of

$$p = gt, \quad d = ct + \frac{1}{2}ft^2, \quad c = 2.5 \text{ ft./sec.}$$

and

$$f = \frac{1}{4} \text{ ft./sec.}^2$$

Thus

$$\theta \rightarrow 64 - \frac{\pi}{4}, \quad \text{as } t \rightarrow \infty.$$

The zeros of  $R_2$  are given by

$$\sin \theta = 0, \quad \text{i.e. } \theta = n\pi,$$

or 
$$\frac{64t}{20+t} = \left(n + \frac{1}{4}\right) \pi = K\pi,$$

where

$$K = n + \frac{1}{4}.$$

This gives

$$t = 20 K\pi / (64 - K\pi).$$

The following table shows the results of numerical calculation:

TABLE II  
Zeros of  $R_2$

	$\overset{+}{\cap}$	$\overset{+}{\cap}$	$\overset{+}{\cap}$	$\overset{+}{\cap}$	$\overset{+}{\cap}$	$\overset{+}{\cap}$	$\overset{+}{\cap}$	$\overset{+}{\cap}$	$\overset{+}{\cap}$	$\overset{+}{\cap}$	$\overset{+}{\cap}$	$\overset{+}{\cap}$
$n$	4	5	6	7	8	9	10	11	12	13	14	15
$t$	5.3	6.9	8.8	11	13.6	16.6	20.2	24.7	32.2	37.2	46.5	59.5
		$\cup$		$\cup$		$\cup$		$\cup$		$\cup$		$\cup$

The number of fluctuations in a specified interval of time gradually diminishes with time and ultimately for a large time the motion is without fluctuation. The wave length of the fluctuation increases with time.

$R_2$  is positive between 5.3 and 6.9 seconds, and negative between 6.9 and 8.8 seconds, etc. This is shown by signs like  $\overset{+}{\cap}$  and  $\cup$ . Assuming that maximum positive and negative amplitudes occur roughly half-way between two consecutive zeros and reading these extremum values from the graphs of  $\pm R_2$  we get the following table for the humps and hollows of  $R_2$ .

TABLE III  
Humps and Hollows of  $R_2$

$t$	6.1	7.9	9.9	12.3	15.1	18.4	22.5	27.5	33.7	41.9	53
$R_2$ (extremum)	+1.6	-1.8	+2.2	-2.5	+3	-3.5	+4.2	-5.2	+6.6	-8.1	+10.6

With the help of this table and table II the actual graph of  $R_2$  can be drawn. This is shown in Fig. 2.

### 7. Total resistance

The total resistance is

$$R = R_1 + R_2 + R_3.$$

From Table I the graph of  $R_1 + R_3$  is drawn (shown in Fig. 3).  $R_2$  has been superposed with the help of tables II and III on the graph of  $R_1 + R_3$ .  $R_2$  represents a sort of perturbation effect on  $R_1 + R_3$ .

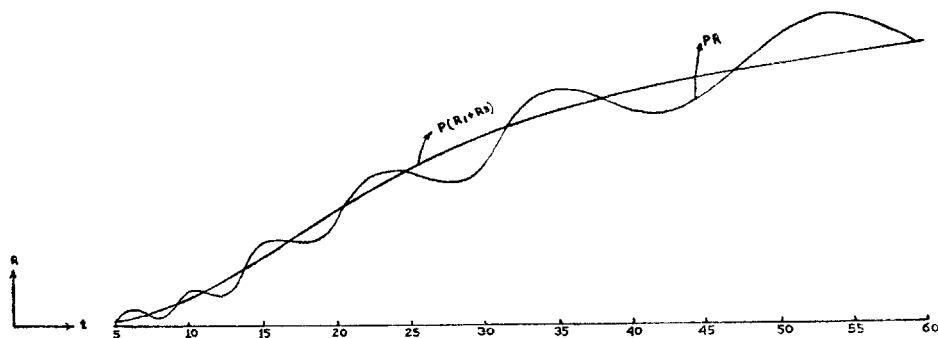


FIG. 3.

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## ABSTRACT

In an earlier paper the surface wave produced by the uniformly accelerated motion of a pressure system over the undisturbed surface of deep water was worked out in the form of an infinite repeated integral which was evaluated by Kelvin's method of group approximation. The wave resistance corresponding to these waves has been worked out in the present paper. It consists of three parts,  $R_1$ ,  $R_2$  and  $R_3$ .  $R_3$  represents the direct effect of acceleration;  $R_1$  and  $R_2$  are analogous to Havelock's results (1917) for uniform motion of a pressure system.  $R_2$  in any case is small, while  $R_3$ , due to acceleration, is more prominent than the other two components.

## REFERENCES

- Bhattacharya, R. N. (1956). Waves produced by a pressure system moving with an acceleration over the surface of deep water. *PNISIPS*, **22**, 155-169.  
 Havelock, T. H. (1917). The Initial Wave Resistance of a Moving Pressure system. *Proc. Roy. Soc., A*, **93**, 240-253.  
 Lamb, H. (1932). *Hydrodynamics* (6th Edn.), 395-396.

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