

A NEW METHOD FOR THE CALCULATION OF THERMAL CONDUCTIVITY OF BINARY GAS MIXTURES

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A new method for calculating the thermal conductivities of binary gas mixtures has been suggested on the basis of Eucken approximation and applied for six monoatomic non-polar and six other gas mixtures. The essential feature of the present method is that it avoids the use of experimental thermal conductivity values of gaseous mixtures as well as the viscosity of pure components. There is no need of adjustment for the best experimental fit. Thermal conductivity values calculated by the present method show good agreement with the experimental values for the twelve gaseous mixtures. The accuracy is of the same order or better than those of Lindsay-Bromley method.

INTRODUCTION

AMONGST the various formulae proposed for calculating the thermal conductivity of gas mixtures, Wassiljewa equation (Wassiljewa, 1904) has been found to be the most successful and has theoretical justification. Wassiljewa expression

$$\lambda_{\text{mix}} = \frac{\lambda_i}{1 + A_{ij} \frac{X_j}{X_i}} + \frac{\lambda_j}{1 + A_{ji} \frac{X_i}{X_j}} \quad \dots(1)$$

has two adjustable parameters A_{ij} and A_{ji} . A_{ij} is interpreted (Cowling, 1961; Wright & Gray, 1962; Cowling *et al.*, 1963) as the ratio of the efficiencies with which molecules j and i respectively impede the transport of heat by molecules i . Accurate estimation of Wassiljewa coefficients is the main problem in the theoretical evaluation of λ_{mix} of gases. Some workers (Gray *et al.*, 1969, 1970; Maczek & Gray, 1969, 1970) have computed the values of A_{ij} and A_{ji} for a large number of pairs utilizing the experimental data of λ_{mix} , λ_i , and λ_j . Out of all the pairs computed only those are selected which give the smallest algebraic mean deviation from experimental values. Such selected values of A_{ij} and A_{ji} are thus used for theoretical calculations of thermal conductivity of binary mixtures from eqn. (1). In addition, some workers (Saksena & Saxena, 1965) have used experimental values of λ_{mix} for gaseous mixtures around the middle composition to calculate the Wassiljewa coefficients and thus got the good agreement between calculated and experimental values of λ_{mix} . In both the approaches, the experimental values of λ_{mix} are required beforehand, without which the theoretical

evaluation of thermal conductivities is not possible. On the other hand several empirical formulae for A_{ij} have also been proposed. Best estimates of A_{ij} for both polar and non-polar gases may be made from the empirical equation of Lindsay and Bromley (1950) in terms of viscosity η , Sutherland's constant S and the molecular weight M of the pure gases

$$A_{ij} = \frac{1}{4} \left[1 + \left\{ \frac{\eta_i}{\eta_j} \left(\frac{M_j}{M_i} \right)^{3/4} \frac{T + S_i}{T + S_j} \right\}^{1/2} \right]^2 \left(\frac{T + S_{ij}}{T + S_i} \right), \quad \dots(2)$$

where $S_{ij} = (S_i S_j)^{1/2}$ if both the components i and j are non-polar and $S_{ij} = 0.73 (S_i S_j)^{1/2}$ if one or both the components is polar. Although Lindsay-Bromley method does not require the knowledge of experimental λ_{mix} values, yet in experimental viscosity data of the pure components are needed for the evaluation of A_{ij} .

In the present paper, the authors are suggesting a new method which enables the calculation of thermal conductivities of binary gas mixtures at all compositions and temperatures.

In this method, the experimental thermal conductivity values are not needed for the calculation of A_{ij} . Unlike the Lindsay-Bromley method which has been widely used, the present approach avoids the use of experimental viscosity data of pure components. In addition, the proposed equation is simpler for binary monoatomic gas mixture and $(M_i/M_j)^{3/4}$ term is reduced to $(M_i/M_j)^{1/4}$. In spite of unadjustment of Wassiljewa coefficients for best experimental fit, the present method yields the results of almost same accuracy as obtained by the other traditional methods. Thermal conductivities of following pairs have been calculated and compared utilizing the present approach : Kr + Ar ; Kr + Ne ; Kr + He ; Ar + Ne ; Ne + He ; Ar + He ; and Ne + He at 18 °C and CH₄ + SO₂ ; N₂O + SO₂ ; CO₂ + SO₂ ; Ar + SO₂ ; NH₃ + N₂O ; and H₂ + O₂ at 50 and 100 °C.

THEORETICAL

Eucken has given the first approximation to the thermal conductivity of a pure gas component, which related thermal conductivity to the viscosity of the gas in the following way

$$\lambda_1 = \frac{15R}{4M} \left(\frac{4C_V}{15R} + \frac{3}{5} \right) \eta_1 \quad \dots(3)$$

where λ_1 and η_1 are the coefficients of thermal conductivity and viscosity respectively, each to the first approximation, C_V the molar heat capacity at constant volume, R the molar gas constant and M and molecular weight of the gas. This is applicable to polyatomic gases where the molecules have rotational and vibrational energies in addition to the kinetic energy of translation and these energies may be exchanged in collision. For binary monoatomic gas mixtures C_V and R terms for one component can be taken approximately equal to those for the other component and the following form is applicable to monoatomic gases only :

$$\lambda_1 = \frac{15R}{4M} \eta_1. \quad \dots(4)$$

From eqn. (3), the relation for binary polyatomic gas mixture is

$$\frac{[\eta_i]_1}{[\eta_j]_1} = \frac{M_i \left[\frac{4}{15} C_{V_i} + \frac{3}{5} R_i \right] [\lambda_i]_1}{M_j \left[\frac{4}{15} C_{V_j} + \frac{3}{5} R_j \right] [\lambda_j]_1} \quad \dots(5)$$

and the following relation is obtained for binary polyatomic gas mixture

$$\frac{[\eta_i]_1}{[\eta_j]_1} = \frac{M_i}{M_j} \frac{[\lambda_i]_1}{[\lambda_j]_1} \quad \dots(6)$$

The approximation

$$\frac{[\eta_i]_1}{[\eta_j]_1} \approx \frac{\eta_i}{\eta_j} \text{ and } \frac{[\lambda_i]_1}{[\lambda_j]_1} \approx \frac{\lambda_i}{\lambda_j} \quad \dots(7)$$

can be taken here for purposes of calculation.

From eqns. (2), (5), and (7) Wassiljewa coefficients A_{ij} and A_{ji} for binary polyatomic gas mixtures are given by

$$A_{ij} = \frac{1}{4} \left[1 + \left\{ \frac{\lambda_i}{\lambda_j} \left(\frac{M_i}{M_j} \right)^{1/4} \frac{\frac{4}{15} C_{V_i} + \frac{3}{5} R_i}{\frac{4}{15} C_{V_j} + \frac{3}{5} R_j} \frac{T + S_i}{T + S_j} \right\}^{\frac{1}{2}} \right]^2 \frac{T + S_{ij}}{T + S_i} \quad \dots(8)$$

and

$$A_{ji} = \frac{1}{4} \left[1 + \left\{ \frac{\lambda_j}{\lambda_i} \left(\frac{M_j}{M_i} \right)^{1/4} \frac{\frac{4}{15} C_{V_i} + \frac{3}{5} R_i}{\frac{4}{15} C_{V_j} + \frac{3}{5} R_j} \frac{T + S_j}{T + S_i} \right\}^{\frac{1}{2}} \right]^2 \frac{T + S_{ji}}{T + S_j} \quad \dots(9)$$

Similarly from eqns. (2), (6), and (7), Wassiljewa coefficients for binary monoatomic gas mixtures can be written as

$$A_{ij} = \frac{1}{4} \left[1 + \left\{ \frac{\lambda_i}{\lambda_j} \left(\frac{M_i}{M_j} \right)^{1/4} \frac{T + S_i}{T + S_j} \right\}^{1/2} \right]^2 \frac{T + S_{ij}}{T + S_i} \quad \dots(10)$$

and

$$A_{ji} = \frac{1}{4} \left[1 + \left\{ \frac{\lambda_j}{\lambda_i} \left(\frac{M_j}{M_i} \right)^{1/4} \frac{T + S_j}{T + S_i} \right\}^{1/2} \right]^2 \frac{T + S_{ji}}{T + S_j}, \quad \dots(11)$$

where all the terms have the same significances as explained earlier. For the mixture of one monoatomic and the other polyatomic gases, Wassiljewa coefficients can also be derived from eqns. (2), (3), (4), and (7).

METHOD OF CALCULATION

For each system Wasiljewa coefficient A_{ij} and A_{ji} have been calculated from eqns. (8),(9),(10) and (11) To calculate molar heat capacity at constant volume C_V terms, we

first calculate molar heat capacity at constant pressure C_p terms is calculated from the well-known relation.

$$C_p = \alpha + \beta T + \gamma T^2 + \delta T^3, \quad \dots(12)$$

where α , β , γ , and δ are constants depending upon the nature of the gas. These constants are taken from the sources (Spencer *et al.*, 1934, 1942, 1945; Bryant, 1973). These C_p terms are then converted into C_V terms. The experimental values of the coefficients of thermal conductivity of pure components and those of mixtures at varying compositions are taken from the literature (Gray & Holland, 1969; Maczek & Gray, 1970; Thornton, 1961; Thornton & Baker, 1962). The values of Sutherland's constants and molar gas constants have been taken from the reference (Chapman & Cowling, 1970). These A_{ij} values are substituted in Wassiljewa eqn. (1) for getting the thermal conductivities of the binary gas mixtures at different compositions. The percentage deviations from the experimental values are also calculated and compared with those obtained by Lindsay-Bromley equation.

RESULTS AND DISCUSSION

Calculated values of thermal conductivity of six binary monoatomic gas mixtures : Kr + Ar ; Kr + Ne ; Kr + He; Ar + Ne ; Ar + He; and Ne + He at 18 °C, using eqns. (10), (11), and (1) are presented in Table I. For comparison,

TABLE I
Thermal conductivities λ (10^{-7} cal cm $^{-1}$ sec $^{-1}$ °K $^{-1}$) of binary monoatomic gas mixtures at 18 °C

| System $i + j$ | mole fraction X_i | Exptl. (λ) | Wassiljewa + Lindsay - Bromley | | Wassiljewa + The Present method | |
|-----------------------------|-----------------------------|----------------------|--------------------------------|--------|---------------------------------|--------|
| | | | (λ) | % dev. | (λ) | % dev. |
| Kr + Ar | 0.865 | 233 | 241.491 | +3.64 | 241.288 | +3.56 |
| | 0.777 | 242 | 256.193 | +5.86 | 255.881 | +5.74 |
| | 0.673 | 256 | 274.320 | +7.16 | 273.893 | +6.99 |
| | 0.546 | 277 | 297.648 | +7.45 | 297.148 | +7.27 |
| | 0.443 | 302 | 317.608 | +5.17 | 317.090 | +5.00 |
| | 0.330 | 326 | 340.670 | +4.50 | 340.177 | +4.35 |
| | 0.228 | 348 | 362.615 | +4.20 | 362.210 | +4.08 |
| | 0.109 | 387 | 389.683 | +0.69 | 389.353 | +0.61 |
| | Mean absolute deviation (%) | | | +4.83 | | +4.70 |
| Kr + Ne | 0.889 | 257 | 274.998 | +7.00 | 274.665 | +6.87 |
| | 0.797 | 305 | 325.781 | +6.81 | 325.158 | +6.57 |
| | 0.647 | 400 | 420.797 | +5.20 | 419.753 | +4.94 |
| | 0.533 | 482 | 505.526 | +4.88 | 504.216 | +4.61 |
| | 0.438 | 568 | 586.465 | +3.25 | 585.000 | +2.99 |
| | 0.339 | 650 | 683.120 | +5.10 | 681.556 | +4.85 |
| | 0.229 | 780 | 808.878 | +3.70 | 807.412 | +3.51 |
| | 0.111 | 960 | 971.672 | +1.22 | 970.679 | +1.11 |
| | 0.065 | 1030 | 1044.946 | +1.45 | 1044.222 | +1.38 |
| Mean absolute deviation (%) | | | | +4.29 | | +4.09 |

(Continued)

TABLE I — (Continued)

| System $i + j$ | mole fraction (X_i) | Exptl. (λ) | Wassiljewa + Lindsay - Bromley | | Wassiljewa + The Present method | |
|-----------------------------|-----------------------------|----------------------|--------------------------------|--------|---------------------------------|--------|
| | | | (λ) | % dev. | (λ) | % dev. |
| Kr + He | 0.891 | 343 | 337.747 | -1.53 | 338.742 | -1.24 |
| | 0.797 | 480 | 456.246 | -4.95 | 458.148 | -4.55 |
| | 0.698 | 642 | 602.576 | -6.14 | 605.474 | -5.69 |
| | 0.600 | 825 | 775.340 | -6.02 | 779.314 | -5.54 |
| | 0.439 | 1210 | 1144.374 | -5.42 | 1150.089 | -4.95 |
| | 0.353 | 1530 | 1404.042 | -8.23 | 1410.568 | -7.81 |
| | 0.272 | 1850 | 1797.190 | -2.85 | 1803.706 | -2.50 |
| | 0.151 | 2500 | 2317.513 | -7.30 | 2324.071 | -7.04 |
| | 0.069 | 3050 | 2899.396 | -4.94 | 2903.923 | -4.90 |
| | Mean absolute deviation (%) | | | -5.26 | | -4.91 |
| Ar + Ne | 0.900 | 470 | 465.667 | -0.92 | 465.394 | -0.98 |
| | 0.803 | 520 | 517.458 | -0.49 | 516.936 | -0.59 |
| | 0.726 | 570 | 561.415 | -1.51 | 560.722 | -1.63 |
| | 0.638 | 620 | 615.749 | -0.69 | 614.160 | -0.94 |
| | 0.541 | 680 | 678.896 | -0.17 | 677.793 | -0.32 |
| | 0.436 | 760 | 754.048 | -0.78 | 752.952 | -0.93 |
| | 0.328 | 840 | 839.184 | -0.10 | 836.065 | -0.47 |
| | 0.221 | 930 | 932.443 | +0.26 | 931.469 | +0.16 |
| | 0.157 | 990 | 993.164 | +0.31 | 992.298 | +0.23 |
| | Mean absolute deviation (%) | | | -0.45 | | -0.61 |
| Ar + He | 0.914 | 540 | 524.264 | -2.91 | 529.296 | -1.98 |
| | 0.844 | 630 | 645.572 | +2.47 | 631.177 | +0.19 |
| | 0.782 | 730 | 724.159 | -0.80 | 729.690 | -0.04 |
| | 0.720 | 830 | 829.960 | 0.00 | 837.105 | +0.98 |
| | 0.645 | 960 | 971.691 | +1.22 | 980.753 | +2.16 |
| | 0.574 | 1110 | 1122.052 | +1.09 | 1132.881 | +2.06 |
| | 0.520 | 1270 | 1248.797 | -1.67 | 1260.880 | -0.72 |
| | 0.438 | 1510 | 1465.617 | -2.94 | 1479.342 | -2.03 |
| | 0.299 | 2040 | 1919.690 | -5.90 | 1935.013 | -5.15 |
| | 0.208 | 2410 | 2297.343 | -4.67 | 2312.117 | -4.89 |
| | 0.061 | 3300 | 3112.494 | -5.68 | 3120.494 | -5.44 |
| Mean absolute deviation (%) | | | | -1.80 | | -1.36 |
| Ne + He | 0.894 | 1330 | 1330.172 | +0.01 | 1332.586 | +0.19 |
| | 0.783 | 1530 | 1523.363 | -0.43 | 1528.071 | -0.13 |
| | 0.655 | 1790 | 1767.888 | -1.23 | 1774.845 | -0.85 |
| | 0.565 | 1990 | 1955.672 | -1.72 | 1963.831 | -1.31 |
| | 0.393 | 2370 | 2357.285 | -0.54 | 2366.447 | -0.15 |
| | 0.250 | 2840 | 2742.191 | -3.44 | 2750.403 | -3.15 |
| | 0.158 | 3100 | 3019.232 | -2.61 | 3025.646 | -2.40 |
| Mean absolute deviation (%) | | | | -1.42 | | -1.11 |

the experimental values of λ_{mix} for these pairs as well as the theoretically calculated values obtained from Lindsay-Bromley eqn. (2) are also enlisted. Percentage deviations and mean absolute deviation for each pair are shown in the Table. Similarly

eqns. (8), (9), and (1) are used to evaluate the thermal conductivities of four polyatomic gas mixtures (one polar component) : $\text{CH}_4 + \text{SO}_2$; $\text{N}_2\text{O} + \text{SO}_2$; $\text{CO}_2 + \text{SO}_2$, and $\text{NH}_3 + \text{N}_2\text{O}$; one monoatomic and other polyatomic polar ($\text{Ar} + \text{SO}_2$), and one pair containing both diatomic and non-polar ($\text{H}_2 + \text{O}_2$) at 50° and 100 °C. These values in conjunction with experimental and theoretical Lindsay-Bromley values are enlisted in Table II. Percentage deviations and mean absolute deviations from ex-

TABLE II

Thermal conductivities λ (Cal km⁻¹ sec⁻¹ °K⁻¹) of binary gas mixtures.

| System $i + j$ | Mole fraction (X_i) | Exptl. (λ) | Wassiljewa + Lindsay - Bromley | | Wassiljewa + The Present method | |
|------------------------------------|-------------------------|----------------------|--------------------------------|--------|---------------------------------|--------|
| | | | (λ) | % dev. | (λ) | % dev. |
| <i>At 50 °C</i> | | | | | | |
| $\text{CH}_4 + \text{SO}_2$ | 0.1030 | 2.98 | 3.051 | + 2.39 | 3.021 | + 1.39 |
| | 0.2005 | 3.48 | 3.584 | + 2.99 | 3.529 | + 1.23 |
| | 0.2980 | 3.98 | 4.141 | + 4.04 | 4.066 | + 2.15 |
| | 0.4010 | 4.575 | 4.757 | + 3.99 | 4.665 | + 1.98 |
| | 0.4995 | 5.205 | 5.375 | + 3.26 | 5.273 | + 1.31 |
| | 0.6020 | 5.87 | 6.046 | + 3.01 | 5.943 | + 1.25 |
| | 0.7025 | 6.52 | 6.736 | + 3.31 | 6.640 | + 1.84 |
| | 0.8005 | 7.304 | 7.435 | + 1.80 | 7.444 | + 1.91 |
| | 0.8995 | 8.045 | 8.169 | + 1.55 | 8.123 | + 0.97 |
| Mean absolute deviation (%) | | | | + 2.93 | | + 1.56 |
| <i>At 100 °C</i> | | | | | | |
| $\text{CH}_4 + \text{SO}_2$ | 0.1030 | 3.65 | 3.729 | + 2.16 | 3.683 | + 0.90 |
| | 0.2005 | 4.195 | 4.380 | + 4.41 | 4.296 | + 2.40 |
| | 0.2980 | 4.81 | 5.059 | + 5.17 | 4.942 | + 2.75 |
| | 0.4010 | 5.85 | 5.807 | + 4.07 | 5.665 | + 1.53 |
| | 0.4995 | 6.305 | 6.553 | + 3.94 | 6.397 | + 1.47 |
| | 0.6020 | 7.05 | 7.363 | + 4.44 | 7.204 | + 2.19 |
| | 0.7025 | 7.835 | 8.189 | + 4.52 | 8.042 | + 2.65 |
| | 0.8005 | 8.80 | 9.026 | + 2.57 | 8.907 | + 1.21 |
| | 0.8995 | 9.745 | 9.900 | + 1.59 | 9.829 | + 0.86 |
| Mean absolute deviation (%) | | | | + 3.65 | | + 1.77 |
| <i>At 50 °C</i> | | | | | | |
| $\text{N}_2\text{O} + \text{SO}_2$ | 0.101 | 2.72 | 2.760 | + 1.48 | 2.752 | + 1.16 |
| | 0.199 | 2.925 | 2.994 | + 2.35 | 3.979 | + 1.85 |
| | 0.301 | 3.125 | 3.230 | + 3.37 | 3.211 | + 2.76 |
| | 0.402 | 3.355 | 3.456 | + 3.02 | 3.435 | + 2.39 |
| | 0.507 | 3.65 | 3.681 | + 3.27 | 3.660 | + 2.67 |
| | 0.601 | 3.75 | 3.873 | + 3.28 | 3.853 | + 2.75 |
| | 0.702 | 3.95 | 4.066 | + 2.93 | 4.049 | + 2.51 |
| | 0.800 | 4.175 | 4.238 | + 1.51 | 4.226 | + 1.23 |
| | 0.9025 | 4.36 | 4.400 | + 0.91 | 4.394 | + 0.78 |
| Mean absolute deviation (%) | | | | + 2.46 | | + 2.01 |

(Continued)

TABLE II — (Continued)

| System $i + j$ | mole fraction (X_i) | Exptl. (λ) | Wassiljewa + Lindsay - Bromley | | Wassiljewa + The Present method | |
|------------------------------------|-------------------------|----------------------|--------------------------------|--------|---------------------------------|--------|
| | | | (λ) | % dev. | (λ) | % dev. |
| <i>At 100 °C</i> | | | | | | |
| N ₂ O + SO ₂ | 0.101 | 3.335 | 3.369 | + 1.02 | 3.349 | + 0.43 |
| | 0.199 | 3.59 | 3.652 | + 1.72 | 3.618 | + 0.77 |
| | 0.301 | 3.815 | 3.937 | + 3.19 | 3.892 | + 2.02 |
| | 0.402 | 4.095 | 4.208 | + 2.76 | 4.157 | + 1.53 |
| | 0.507 | 4.34 | 4.477 | + 3.15 | 4.425 | + 1.97 |
| | 0.601 | 4.58 | 4.705 | + 2.72 | 4.656 | + 1.67 |
| | 0.702 | 4.805 | 4.933 | + 2.67 | 4.892 | + 1.82 |
| | 0.800 | 5.025 | 5.138 | + 2.24 | 5.108 | + 1.64 |
| | 0.9025 | 5.27 | 5.330 | + 1.13 | 5.314 | + 0.83 |
| Mean absolute deviation (%) | | | | + 2.29 | | + 1.41 |
| <i>At 50 °C</i> | | | | | | |
| CO ₂ + SO ₂ | 0.100 | 2.70 | 2.745 | + 1.65 | 2.736 | + 1.33 |
| | 0.2195 | 2.935 | 3.012 | + 2.62 | 2.995 | + 2.06 |
| | 0.303 | 3.12 | 3.192 | + 2.31 | 3.172 | + 1.67 |
| | 0.400 | 3.30 | 3.394 | + 2.84 | 3.371 | + 2.16 |
| | 0.501 | 3.50 | 3.593 | + 2.67 | 3.570 | + 2.01 |
| | 0.6025 | 3.665 | 3.782 | + 3.19 | 3.760 | + 2.60 |
| | 0.699 | 3.845 | 3.947 | + 2.66 | 3.929 | + 2.19 |
| | 0.801 | 4.02 | 4.106 | + 2.14 | 4.093 | + 1.81 |
| | 0.9015 | 4.20 | 4.243 | + 1.02 | 4.236 | + 0.85 |
| Mean absolute deviation (%) | | | | + 2.34 | | + 1.85 |
| <i>At 100 °C</i> | | | | | | |
| CO ₂ + SO ₂ | 0.100 | 3.31 | 3.348 | + 1.16 | 3.332 | + 0.66 |
| | 0.2195 | 3.575 | 3.670 | + 2.66 | 3.640 | + 1.82 |
| | 0.303 | 3.785 | 3.887 | + 1.69 | 3.850 | + 1.72 |
| | 0.400 | 4.01 | 4.130 | + 2.98 | 4.088 | + 1.95 |
| | 0.501 | 4.26 | 4.370 | + 2.58 | 4.328 | + 1.59 |
| | 0.6025 | 4.47 | 4.597 | + 2.84 | 4.557 | + 1.95 |
| | 0.699 | 4.685 | 4.797 | + 2.39 | 4.763 | + 1.68 |
| | 0.801 | 4.90 | 4.983 | + 2.70 | 4.966 | + 1.34 |
| | 0.9015 | 5.10 | 5.158 | + 1.15 | 5.145 | + 0.88 |
| Mean absolute deviation (%) | | | | + 2.24 | | + 1.51 |
| <i>At 50 °C</i> | | | | | | |
| Ar + SO ₂ | 0.102 | 2.66 | 2.713 | + 1.98 | 2.704 | + 1.65 |
| | 0.200 | 2.825 | 3.908 | + 2.94 | 2.892 | + 2.38 |
| | 0.3015 | 2.98 | 3.115 | + 4.52 | 3.092 | + 3.78 |
| | 0.4005 | 3.17 | 3.319 | + 4.72 | 3.293 | + 3.87 |
| | 0.501 | 3.37 | 3.529 | + 4.73 | 3.500 | + 3.85 |
| | 0.601 | 3.56 | 3.738 | + 5.01 | 3.708 | + 4.15 |
| | 0.6985 | 3.785 | 3.939 | + 4.07 | 3.910 | + 3.31 |
| | 0.7995 | 4.02 | 4.140 | + 2.98 | 4.116 | + 2.40 |
| | 0.9005 | 4.25 | 4.327 | + 1.82 | 4.314 | + 1.50 |
| Mean absolute deviation (%) | | | | + 3.64 | | + 2.99 |

TABLE II — (Continued)

| System $i + j$ | mole fraction (X_i) | Exptl. (λ) | Wassijlewa + Lindsay - Bromley | | Wassiljewa + The Present method | |
|------------------------------------|-----------------------------|----------------------|--------------------------------|--------|---------------------------------|--------|
| | | | (λ) | % dev. | (λ) | % dev. |
| At 100 °C | | | | | | |
| Ar + SO ₂ | 0.102 | 3.25 | 3.275 | + 0.76 | 3.273 | + 0.72 |
| | 0.200 | 3.405 | 3.475 | + 2.05 | 3.472 | + 1.96 |
| | 0.3015 | 3.57 | 3.685 | + 3.23 | 3.681 | + 3.11 |
| | 0.4005 | 3.77 | 3.892 | + 3.25 | 3.888 | + 3.12 |
| | 0.501 | 3.96 | 4.103 | + 3.61 | 4.098 | + 3.47 |
| | 0.601 | 4.155 | 4.311 | + 3.75 | 4.305 | + 2.92 |
| | 0.6985 | 4.365 | 4.509 | + 3.29 | 4.504 | + 3.18 |
| | 0.7995 | 4.575 | 4.705 | + 2.83 | 4.701 | + 2.75 |
| | 0.9005 | 4.795 | 4.886 | + 1.90 | 4.884 | + 1.85 |
| | Mean absolute deviation (%) | | | + 2.74 | | + 2.56 |
| At 50 °C | | | | | | |
| NH ₃ + N ₂ O | 0.0905 | 4.795 | 4.793 | - 0.04 | 4.822 | + 0.57 |
| | 0.202 | 5.085 | 5.099 | + 0.27 | 5.151 | + 1.30 |
| | 0.301 | 5.315 | 5.349 | + 0.65 | 5.418 | + 1.93 |
| | 0.401 | 5.525 | 5.586 | + 1.11 | 5.661 | + 2.46 |
| | 0.4805 | 5.715 | 5.761 | + 0.80 | 5.835 | + 1.09 |
| | 0.5985 | 5.93 | 5.994 | + 1.07 | 6.060 | + 2.19 |
| | 0.700 | 6.11 | 6.166 | + 0.92 | 6.219 | + 1.79 |
| | 0.799 | 6.245 | 6.306 | + 0.98 | 6.343 | + 1.57 |
| | 0.873 | 6.365 | 6.390 | + 0.40 | 6.414 | + 0.77 |
| | Mean absolute deviation (%) | | | + 0.68 | | + 1.63 |
| At 100 °C | | | | | | |
| NH ₃ + N ₂ O | 0.0905 | 5.775 | 5.802 | + 0.46 | 5.839 | + 1.12 |
| | 0.202 | 6.175 | 6.172 | - 0.05 | 6.245 | + 1.13 |
| | 0.301 | 6.46 | 6.484 | + 0.38 | 6.577 | + 1.81 |
| | 0.401 | 6.77 | 6.782 | + 0.18 | 6.884 | + 1.69 |
| | 0.4805 | 6.985 | 7.005 | + 0.28 | 7.108 | + 1.77 |
| | 0.5985 | 7.26 | 7.308 | + 0.66 | 7.404 | + 1.98 |
| | 0.700 | 7.47 | 7.541 | + 0.95 | 7.622 | + 2.03 |
| | 0.799 | 7.685 | 7.739 | + 0.71 | 7.798 | + 1.48 |
| | 0.873 | 7.82 | 7.867 | + 0.16 | 7.906 | + 1.11 |
| | Mean absolute deviation (%) | | | + 0.47 | | + 1.57 |
| At 50 °C | | | | | | |
| H ₂ + O ₂ | 0.1143 | 9.08 | 9.12 | + 0.5 | 9.125 | + 0.49 |
| | 0.2262 | 11.53 | 11.70 | + 1.4 | 11.706 | + 1.52 |
| | 0.3944 | 15.79 | 16.25 | + 2.9 | 16.267 | + 3.02 |
| | 0.5033 | 19.43 | 19.76 | + 1.7 | 19.771 | + 1.76 |
| | 0.6092 | 22.92 | 23.70 | + 3.4 | 23.710 | + 3.45 |
| | 0.7168 | 27.91 | 28.38 | + 1.7 | 28.382 | + 1.69 |
| | 0.8320 | 33.77 | 34.36 | + 1.8 | 34.340 | + 1.69 |
| | 0.8783 | 36.58 | 37.12 | + 1.5 | 37.082 | + 1.37 |
| | Mean absolute deviation (%) | | | + 1.86 | | + 1.87 |

(Continued)

At 100°C

| | | | | | | |
|-----------------------------|--------|-------|-------|--------|--------|---------|
| $H_2 + O_2$ | 0.1143 | 10.19 | 10.26 | + 0.6 | 10.279 | + 0.87 |
| | 0.2262 | 13.01 | 13.10 | + 0.7 | 13.141 | + 1.01 |
| | 0.3944 | 17.80 | 18.13 | + 1.9 | 18.202 | + 22.26 |
| | 0.5033 | 21.91 | 22.01 | + 0.5 | 22.093 | + 0.84 |
| | 0.6092 | 25.80 | 26.39 | + 2.3 | 26.467 | + 2.58 |
| | 0.7168 | 31.37 | 31.59 | + 0.7 | 31.658 | + 0.92 |
| | 0.8320 | 37.70 | 38.25 | + 1.4 | 38.283 | + 1.55 |
| | 0.8783 | 40.72 | 41.32 | + 1.5 | 41.333 | + 1.51 |
| Mean absolute deviation (%) | | | | + 1.20 | | + 1.44 |

perimental values for the present method and Lindsay-Bromley method are shown. For the calculation of thermal conductivity of binary gas mixture, the experimental values of thermal conductivities of pure gases are taken from the sources (Gray *et al.*, 1969; Maczek & Gray, 1970; Thornton, 1961; Thornton & Baker, 1962).

The Wassiljewa coefficient A_{ij} and A_{ji} for binary monoatomic gas mixtures, obtained from present procedure are recorded in Table III and compared with Lindsay-Bromley values. For polyatomic gas mixtures, the presently calculated values of A_{ij} and A_{ji} at two different temperatures 50 and 100°C with Lindsay-Bromley values (Gray *et al.*, 1969; Maczek & Gray, 1970) are presented in Table IV. For monoatomic gas mixtures, Lindsay-Bromley values of Wassiljewa coefficients at 18°C are not available in literature and the values reported have been calculated by us.

Thornton (1961) calculated the thermal conductivities of Kr + Ar; Kr + Ne; and Kr + He and Thornton and Baker (1962) those of Ar + Ne; Ar + He; and Ne + He at 18°C by using L-J(6:12) Potential. Their calculated values show the mean absolute deviations from — 8.07 to + 1.45. Lindsay-Bromley method affords mean absolute deviations from — 5.26 to + 4.83 whereas in the present method the mean absolute deviations are found to be — 4.91 to + 4.70. The mean absolute deviations due to Lindsay-Bromley method and the present method for binary monoatomic gas mixtures are given in Table III. Thus the calculated thermal conductivities of Thornton (1961) and Thornton and Baker (1962) are less than the experimental values while

TABLE III

Wassiljewa coefficients A_{ij} for thermal conductivities of binary monoatomic gas mixtures at 18°C

| System $i + j$ | Lindsay - Bromley method | | | The Present Method | | |
|----------------|--------------------------|----------|--------|--------------------|----------|--------|
| | A_{ij} | A_{ji} | % dev. | A_{ij} | A_{ji} | % dev. |
| Kr + Ar | 0.8074 | 1.2520 | + 4.83 | 0.8030 | 1.2620 | + 4.70 |
| Kr + Ne | 0.5404 | 1.9770 | + 4.29 | 0.5384 | 1.9890 | + 4.09 |
| Kr + He | 0.4262 | 3.2626 | — 5.26 | 0.4277 | 3.2361 | — 4.91 |
| Ar + Ne | 0.6610 | 1.5387 | — 0.45 | 0.6582 | 1.5470 | — 0.61 |
| Ar + He | 0.5019 | 2.4840 | — 1.80 | 0.5065 | 2.4390 | — 1.36 |
| Ne + He | 0.7163 | 1.4990 | — 1.42 | 0.7233 | 1.4790 | — 1.11 |

TABLE IV
Wassiljewa coefficients A_{ij} for thermal conductivities of binary gas mixtures

| System $i + j$ | Temp. (°C) | Lindsay - Bromley method | | | The Present Method | | |
|------------------------------------|---------------|--------------------------|----------|--------|--------------------|----------|--------|
| | | A_{ij} | A_{ji} | % dev. | A_{ij} | A_{ji} | % dev. |
| $\text{CH}_4 + \text{SO}_2$ | 50 | 1.38 | 0.55 | + 2.93 | 1.4602 | 0.5302 | + 1.56 |
| | 100 | 1.35 | 0.57 | + 3.65 | 1.4492 | 0.5459 | + 1.77 |
| $\text{N}_2\text{O} + \text{SO}_2$ | 50 | 1.08 | 0.69 | + 2.46 | 1.1213 | 0.6665 | + 2.01 |
| | 100 | 1.06 | 0.71 | + 2.29 | 1.1293 | 0.6772 | + 1.41 |
| $\text{CO}_2 + \text{SO}_2$ | 50 | 1.07 | 0.69 | + 2.34 | 1.1082 | 0.6729 | + 1.85 |
| | 100 | 1.06 | 0.71 | + 2.24 | 1.1198 | 0.6818 | + 1.51 |
| $\text{Ar} + \text{SO}_2$ | 50 | 1.37 | 0.54 | + 3.64 | 1.4086 | 0.5395 | + 2.99 |
| | 100 | 1.35 | 0.57 | + 2.74 | 1.3577 | 0.5687 | + 2.56 |
| $\text{NH}_3 + \text{N}_2\text{O}$ | 50 | 1.04 | 0.73 | + 0.68 | 0.9482 | 0.7822 | + 1.63 |
| | 100 | 1.06 | 0.74 | + 0.47 | 0.9707 | 0.7815 | + 1.57 |
| $\text{H}_2 + \text{O}_2$ | 50 | 1.972 | 0.578 | + 1.86 | 1.9679 | 0.5780 | + 1.87 |
| | 100 | 1.983 | 0.580 | + 1.20 | 1.9683 | 0.5804 | + 1.44 |

Lindsay-Bromley method and our method render higher values than their calculated values.

For other gaseous mixtures i.e., $\text{CH}_4 + \text{SO}_2$; $\text{N}_2\text{O} + \text{SO}_2$; $\text{CO}_2 + \text{SO}_2$; $\text{Ar} + \text{SO}_2$; $\text{NH}_3 + \text{N}_2\text{O}$ and $\text{H}_2 + \text{O}_2$, the calculated values of thermal conductivities by Lindsay-Bromley method and our method are higher than the experimental values (Gray *et al.*, 1969; Maczek & Gray, 1970). The mean absolute deviations due to Lindsay-Bromley and the present method range from + 0.68 to + 3.64 and + 1.56 to + 2.99 respectively at 50 °C and from + 0.47 to + 3.65 and + 1.41 to + 2.56 respectively at 100 °C. The respective values of mean absolute deviations are shown in Table IV.

CONCLUSION

In order to avoid the adjustment procedure and the beforehand use of the experimental thermal conductivity values of mixtures and viscosity of pure components for the evaluation of Wassiljewa coefficients, an alternative method has been adopted which is applicable to various binary gas mixtures at all compositions and different temperatures. The sign and the magnitude of mean deviations are of the same order as obtained by Lindsay-Bromley method. The overall agreement is very good.

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