

# THE SIMULATION OF THIRD ORDER SYSTEMS WITH A LEADING TIME-CONSTANT BY A SINGLE OPERATIONAL AMPLIFIER—II

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In the previous paper (Wadhwa 1964) on the same topic three basic circuits each employing three capacitors and six resistors and capable of simulating, under certain conditions, third order systems with a leading time-constant were presented. In this paper three more basic circuits for simulating the same type of third order systems are presented. The circuits are analysed, the design formulae obtained and the conditions of their physical realizability discussed.

## INTRODUCTION

In Part I a network capable of simulating the general third order linear systems with only one operational amplifier was presented and the design of three circuits capable of simulating, under certain conditions, third order systems of the type

$$F(S) = - \frac{b_0(b_1S+1)}{a_3S^3+a_2S^2+a_1S+1} \quad \dots \quad (1)$$

was discussed. The purpose of this paper is to present three more basic circuits for simulating the system of (1) with a certain arbitrary choice of resistor values and obtain the design formulae and conditions of their physical realizability.

## THIRD ORDER SYSTEM SIMULATION

Three basic circuits capable of simulating, under certain conditions, the system of (1) are shown in Fig. 1.

Transfer function for the circuit of Fig. 1(a) can be shown to be

$$\frac{E_0}{E_1} = - \frac{\frac{\alpha}{3}(RC_3S+1)}{\frac{\alpha\beta}{3}R^3C_3C_6C_8S^3 + \left[ \frac{(\alpha+2\alpha\beta+2\beta)}{3}R^2C_3C_6 + \frac{\alpha}{3}R^2C_3C_8 + \frac{(\alpha+\alpha\beta+2\beta)}{3}R^2C_6C_8 \right] S^2 + \left[ \frac{1}{3}RC_3 + \frac{(3\alpha+2\alpha\beta+6\beta)}{3}RC_6 + \left( \frac{\alpha+1}{3} \right) RC_8 \right] S + 1} \quad \dots \quad (2)$$

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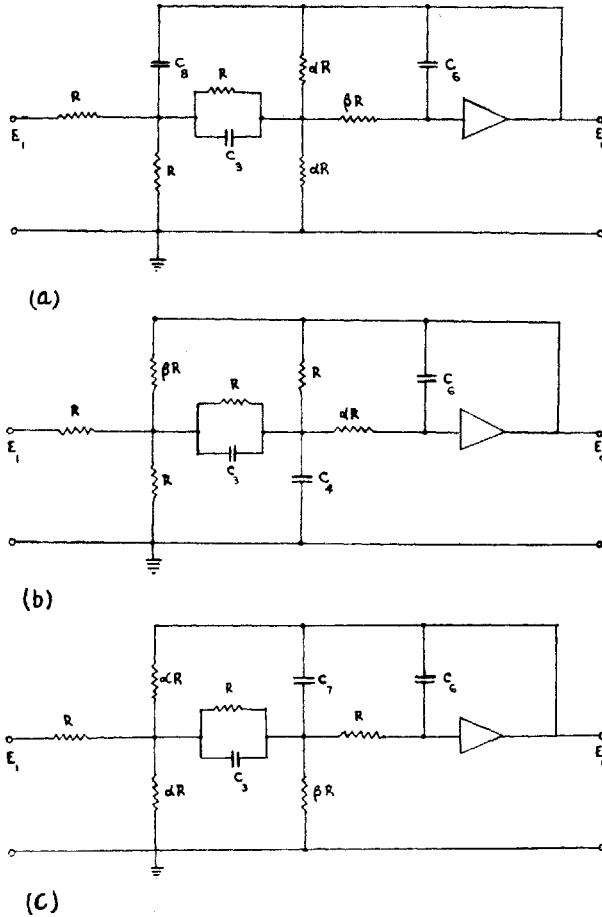


FIG. 1. Networks for the simulation of  $\frac{E_0}{E_1} = -\frac{b_0(b_1S+1)}{a_3S^3+a_2S^2+a_1S+1}$ .

(1) and (2) will be identical if

$$b_0 = \frac{\alpha}{3} \dots \dots \dots (3)$$

$$b_1 = T_3 \dots \dots \dots (4)$$

$$a_1 = \frac{1}{3}T_3 + \frac{(3\alpha + 2\alpha\beta + 6\beta)}{3}T_6 + \left(\frac{\alpha + 1}{3}\right)T_8 \dots \dots (5)$$

$$a_2 = \frac{(\alpha + 2\alpha\beta + 2\beta)}{3}T_3T_6 + \frac{\alpha}{3}T_3T_8 + \frac{(\alpha + \alpha\beta + 2\beta)}{3}T_6T_8 \dots (6)$$

$$a_3 = \frac{\alpha\beta}{3}T_3T_6T_8 \dots \dots \dots (7)$$

where

$$T_n = RC_n \dots \dots \dots (8)$$

Elimination of  $\alpha$ ,  $\beta$ ,  $T_3$  and  $T_6$  from (3) to (7) gives a cubic

$$b_1(1 + 3b)T_8^3 - b_1(3a_1 + 6b_0b_1 - 2b_1)T_8^2 + (9a_2b_1 + b_1^3 - 3a_1b_1^2 - 3a_3)T_8 - 12a_3b_1 = 0 \quad (9)$$

which will have at least one positive real root corresponding to which, as shown in the Appendix, a set of positive real  $\alpha$ ,  $\beta$ ,  $T_3$  and  $T_6$  exists, provided that

$$\left. \begin{aligned} (3a_1 - b_1) &> 0 \\ b_0 b_1 (3a_1 - b_1)^2 &> 24a_3(1 + 3b_0)(1 + b_0) \\ \{3a_2 b_0 b_1 - a_3(2 + 3b_0)\} &> 0 \\ \{3a_2 b_0 b_1 - a_3(2 + 3b_0)\}^2 &> 24a_3 b_0^2 b_1^3 (1 + 3b_0) \end{aligned} \right\} \dots \dots (10)$$

and either

$$OB > OQ > OA > OP \dots \dots \dots (11)$$

or

$$OQ > OB > OP > OA \dots \dots \dots (12)$$

or

$$\left. \begin{aligned} (3a_1 + 6b_0 b_1 - 2b_1) &> 0 \\ (9a_2 b_1 + b_1^3 - 3a_1 b_1^2 - 3a_3) &> 0 \\ \Delta = 4p^3 + 27q^2 &< 0 \end{aligned} \right\} \dots \dots \dots (13)$$

where

$$\left. \begin{aligned} OA &= \frac{b_0 b_1 (3a_1 - b_1) - \sqrt{\Delta_1}}{2b_0 b_1 (1 + 3b_0)} \\ OB &= \frac{b_0 b_1 (3a_1 - b_1) + \sqrt{\Delta_1}}{2b_0 b_1 (1 + 3b_0)} \\ OP &= \frac{3a_2 b_0 b_1 - a_3(2 + 3b_0) - \sqrt{\Delta_2}}{6b_0^2 b_1^2} \\ OQ &= \frac{3a_2 b_0 b_1 - a_3(2 + 3b_0) + \sqrt{\Delta_2}}{6b_0^2 b_1^2} \\ \Delta_1 &= b_0^2 b_1^2 (3a_1 - b_1)^2 - 24a_3 b_0 b_1 (1 + b_0)(1 + 3b_0) \\ \Delta_2 &= \{3a_2 b_0 b_1 - a_3(2 + 3b_0)\}^2 - 24a_3 b_0^2 b_1^3 (1 + 3b_0) \\ p &= \frac{(9a_2 b_1 + b_1^3 - 3a_1 b_1^2 - 3a_3)}{b_1(1 + 3b_0)} - \frac{1}{3} \left( \frac{3a_1 + 6b_0 b_1 - 2b_1}{1 + 3b_0} \right)^2 \\ q &= - \frac{12a_3}{(1 + 3b_0)} + \frac{(3a_1 + 6b_0 b_1 - 2b_1)(9a_2 b_1 + b_1^3 - 3a_1 b_1^2 - 3a_3)}{3b_1(1 + 3b_0)^2} \\ &\quad - \frac{2}{27} \left( \frac{3a_1 + 6b_0 b_1 - 2b_1}{1 + 3b_0} \right)^3 \end{aligned} \right\} \dots (14)$$

Hence, if the inequalities of (10) and either (11) or (12) or (13) are satisfied then at least one positive real set of  $\alpha$ ,  $\beta$ ,  $T_3$ ,  $T_6$  and  $T_8$  exists for which the circuit of Fig. 1(a) is physically realizable. The circuit component values may be obtained by first solving the cubic of (9), and then solving the simultaneous equations (5) and (7) to obtain  $\beta$  and  $T_6$ —as  $\alpha$  and  $T_3$  are known directly from (3) and (4).



where

$$\left. \begin{aligned} k_1 &= (1+3b_0)[2a_3(1+2b_0)+b_0b_1^2(2a_1+b_0b_1)] \\ k_2 &= b_0b_1[4a_2(1+2b_0)+b_1^2(1+3b_0)] \end{aligned} \right\} \dots \dots \dots (28)$$

It is obvious from (24) to (27) that  $\alpha, \beta, T_4$  and  $T_6$  are all real and these will be also positive, if

$$\left. \begin{aligned} 2b_0b_1[a_2(1+3b_0)+b_0b_1^2] &> [2b_0^2b_1^2(2a_1+b_0b_1)+a_3(1+3b_0)^2] \\ (1+3b_0)[2a_3(1+2b_0)+b_0b_1^2(2a_1+b_0b_1)] &> b_0b_1[4a_2(1+2b_0)+b_1^2(1+3b_0)] \end{aligned} \right\} (29)$$

$b_0 < \frac{1}{3}$

Hence, if the inequalities of expression (29) are satisfied then a set of positive real  $\alpha, \beta, T_3, T_4$  and  $T_6$  exists for which the circuit of Fig. 2(b) is physically realizable.

Now, the transfer function for the circuit of Fig. 1(c) can be shown to be

$$\frac{E_0}{E_1} = - \frac{\alpha(RC_3S+1)}{\alpha R^3C_3C_6C_7S^3 + \left[ \frac{(\alpha+2\alpha\beta+2\beta)}{\beta} R^2C_3C_6 + \alpha R^2C_3C_7 + 2(\alpha+1)R^2C_6C_7 \right] S^2 + \left[ RC_3 + \frac{(2\alpha+3\alpha\beta+4\beta+2)}{\beta} RC_6 + 2(\alpha+1)RC_7 \right] S + 1} \dots \dots (30)$$

(1) and (30) will be identical if

$$b_0 = \alpha \dots \dots \dots (31)$$

$$b_1 = T_3 \dots \dots \dots (32)$$

$$a_1 = T_3 + \frac{(2\alpha+3\alpha\beta+4\beta+2)}{\beta} T_6 + 2(\alpha+1)T_7 \dots \dots (33)$$

$$a_2 = \frac{(\alpha+2\alpha\beta+2\beta)}{\beta} T_3T_6 + \alpha T_3T_7 + 2(\alpha+1)T_6T_7 \dots \dots (34)$$

$$a_3 = \alpha T_3T_6T_7 \dots \dots \dots (35)$$

where

$$T_n = RC_n \dots \dots \dots (36)$$

Elimination of  $\alpha, T_3$  and  $T_7$  from (31), (32), (33), (35) and (31), (32), (34), (35) give the following two equations :

$$\frac{1}{\beta} = \frac{1}{2(1+b_0)} \left[ \frac{(a_1-b_1)}{T_6} - \frac{2a_3(1+b_0)}{b_0b_1T_6^2} - (4+3b_0) \right] \dots \dots (37)$$

$$\frac{1}{\beta} = \frac{1}{b_0} \left[ \frac{a_2b_0b_1-2a_3(1+b_0)}{b_0b_1^2T_6} - \frac{a_3}{b_1T_6^2} - 2(1+b_0) \right] \dots \dots (38)$$

which on solution yield

$$\beta = \frac{2(1+b_0)(k'_1-k'_2)^2}{a_1b_0b_1^2(2+b_0)^2(k'_1-k'_2) - b_0b_1^3(2+b_0)^2\{(k'_1-k'_2) + 2a_3(1+b_0)(2+b_0)^2\} - (4+3b_0)(k'_1-k'_2)^2} \quad \dots (39)$$

$$T_6 = \frac{(k'_1-k'_2)}{b_0b_1^2(2+b_0)^2} \quad \dots \quad \dots \quad \dots \quad \dots (40)$$

Since  $\alpha$  and  $T_3$  are known directly from (31) and (32),  $T_7$  may be then obtained from (35)

$$T_7 = \frac{a_3b_1(2+b_0)^2}{(k'_1-k'_2)} \quad \dots \quad \dots \quad \dots \quad \dots (41)$$

where

$$\left. \begin{aligned} k'_1 &= b_0b_1[2a_2(1+b_0) + b_0b_1^2] \\ k'_2 &= a_1b_0^2b_1^2 + 4a_3(1+b_0)^2 \end{aligned} \right\} \quad \dots \quad \dots \quad \dots (42)$$

It is obvious from (39) to (41) that  $\beta$ ,  $T_6$  and  $T_7$  are real and these will be also positive, if

$$(k'_1 - k'_2) > 0$$

and

$$\left. \begin{aligned} [a_1b_0b_1^2(2+b_0)^2(k'_1-k'_2) - b_0b_1^3(2+b_0)^2\{(k'_1-k'_2) + 2a_3(1+b_0)(2+b_0)^2\} - \\ (4+3b_0)(k'_1-k'_2)^2] > 0 \end{aligned} \right\} \quad (43)$$

Hence, if the inequalities of expression (43) are satisfied then a set of positive real  $\alpha$ ,  $\beta$ ,  $T_3$ ,  $T_6$  and  $T_7$  exists for which the circuit of Fig. 1(c) is physically realizable and the circuit component values may be determined with the aid of (31), (32), (39) to (41).

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REFERENCE

Wadhwa, L. K. (1964). The simulation of third order systems with a leading time-constant by a single operational amplifier—I. *Proc. nat. Inst. Sci. India*, A 30, 520-532.



and also real, if

$$b_0 b_1 (3a_1 - b_1)^2 > 24a_3(1 + b_0)(1 + 3b_0). \quad \dots \quad (A.11)$$

Similarly, the curve of (A.7) will cut the  $T_8$ -axis at two points  $P, Q$  whose  $T_8$ -coordinates will be given by

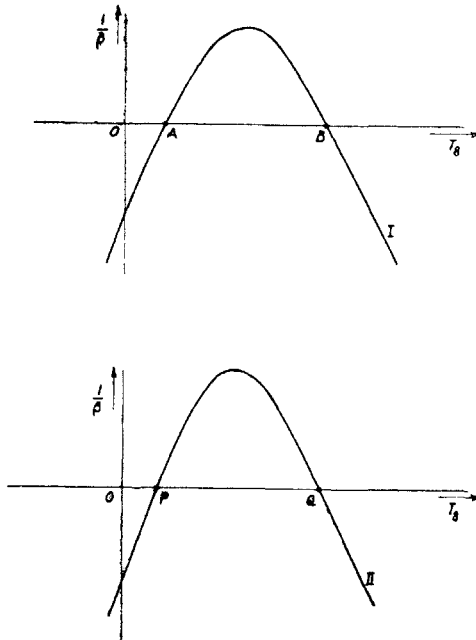
$$T_{8(P, Q)} = \frac{\{3a_2 b_0 b_1 - a_3(2 + 3b_0)\} \pm \sqrt{\{3a_2 b_0 b_1 - a_3(2 + 3b_0)\}^2 - 24a_3 b_0^2 b_1^3 (1 + 3b_0)}}{6b_0^2 b_1^2} \quad \dots \quad (A.12)$$

and these will be positive and real, if

$$\left. \begin{aligned} \{3a_2 b_0 b_1 - a_3(2 + 3b_0)\} &> 0 \\ \{3a_2 b_0 b_1 - a_3(2 + 3b_0)\}^2 &> 24a_3 b_0^2 b_1^3 (1 + 3b_0) \end{aligned} \right\} \quad \dots \quad (A.13)$$

Therefore, if the conditions of expressions (A.10), (A.11) and (A.13) are satisfied then a portion of the curves of (A.6) and (A.7) can exist in the first quadrant and the sketches of these curves for positive  $T_8$  are shown in Fig. 2.

FIG. 2. Sketches of the curves for positive  $T_8$ .



$$\begin{aligned} \text{I} \quad \frac{1}{\beta} &= \frac{b_1}{3a_3} \left[ \left(\frac{3a_1 - b_1}{3}\right) T_8 - \left(\frac{1 + 3b_0}{3}\right) T_8^2 - \frac{2a_3(1 + b_0)}{b_0 b_1} \right] \\ \text{II} \quad \frac{1}{\beta} &= \frac{b_1}{a_3(T_8 + b_1)} \left[ \frac{\{3a_2 b_0 b_1 - a_3(2 + 3b_0)\}}{3b_0 b_1} T_8 - \frac{2a_3(1 + 3b_0)}{3b_0} - b_0 b_1 T_8^2 \right] \end{aligned}$$

Elimination of  $\beta$  from (A.6) and (A.7) gives a cubic

$$b_1(1 + 3b_0)T_8^3 - b_1(3a_1 + 6b_0 b_1 - 2b_1)T_8^2 + (9a_2 b_1 + b_1^3 - 3a_1 b_1^2 - 3a_3)T_8 - 12a_3 b_1 = 0 \quad \dots \quad (A.14)$$



which will have at least one positive and real root; it can have three real roots if its discriminant  $\Delta$  is negative—the sign of the other two roots depending upon the sign of the coefficients of  $T_8$  and  $T_8^2$ .

The real roots of (A.14) give the real points of intersection of the curves of (A.6) and (A.7). Now, the curves will intersect each other in the first quadrant provided that the conditions of (A.10), (A.11) and (A.13) are satisfied, and either

$$OB > OQ > OA > OP \quad \dots \quad \dots \quad \dots \quad (A.15)$$

or

$$OQ > OB > OP > OA \quad \dots \quad \dots \quad \dots \quad (A.16)$$

where

$$OA = \frac{b_0 b_1 (3a_1 - b_1) - \sqrt{b_0^2 b_1^2 (3a_1 - b_1)^2 - 24a_3 b_0 b_1 (1 + b_0)(1 + 3b_0)}}{2b_0 b_1 (1 + 3b_0)}$$

$$OB = \frac{b_0 b_1 (3a_1 - b_1) + \sqrt{b_0^2 b_1^2 (3a_1 - b_1)^2 - 24a_3 b_0 b_1 (1 + b_0)(1 + 3b_0)}}{2b_0 b_1 (1 + 3b_0)}$$

$$OP = \frac{\{3a_2 b_0 b_1 - a_3(2 + 3b_0)\} - \sqrt{\{3a_2 b_0 b_1 - a_3(2 + 3b_0)\}^2 - 24a_3 b_0^2 b_1^3 (1 + 3b_0)}}{6b_0^2 b_1^2}$$

$$OQ = \frac{\{3a_2 b_0 b_1 - a_3(2 + 3b_0)\} + \sqrt{\{3a_2 b_0 b_1 - a_3(2 + 3b_0)\}^2 - 24a_3 b_0^2 b_1^3 (1 + 3b_0)}}{6b_0^2 b_1^2}$$

But, if

$$\left. \begin{aligned} \Delta &= 4p^3 + 27q^2 < 0 \\ (3a_1 + 6b_0 b_1 - 2b_1) &> 0 \\ (9a_2 b_1 + b_1^3 - 3a_1 b_1^2 - 3a_3) &> 0 \end{aligned} \right\} \dots \quad \dots \quad \dots \quad (A.17)$$

where

$$\left. \begin{aligned} p &= \frac{(9a_2 b_1 + b_1^3 - 3a_1 b_1^2 - 3a_3)}{b_1(1 + 3b_0)} - \frac{1}{3} \left( \frac{3a_1 + 6b_0 b_1 - 2b_1}{1 + 3b_0} \right)^2 \\ q &= -\frac{12a_3}{(1 + 3b_0)} + \frac{(3a_1 + 6b_0 b_1 - 2b_1)(9a_2 b_1 + b_1^3 - 3a_1 b_1^2 - 3a_3)}{3b_1(1 + 3b_0)^2} - \frac{2}{27} \left( \frac{3a_1 + 6b_0 b_1 - 2b_1}{1 + 3b_0} \right)^3 \end{aligned} \right\} \dots \quad (A.18)$$

then (A.14) will have three real and positive roots corresponding to which at least one positive real set of  $\alpha$ ,  $\beta$ ,  $T_3$ ,  $T_6$  and  $T_8$  exists, provided that (A.10), (A.11) and (A.13) are also satisfied.

To summarize, if the inequalities of expressions (A.10), (A.11), (A.13) and either (A.15) or (A.16) or (A.17) are satisfied then at least one positive real set of  $\alpha$ ,  $\beta$ ,  $T_3$ ,  $T_6$  and  $T_8$  exists corresponding to which the circuit of Fig. 1(a) is physically realizable.